

10/590627

SF-1148PCT

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IAP9 Rec'd PCT/PTO 24 AUG 2006

DESCRIPTION

MULTILAYER WIRING BOARD

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TECHNICAL FIELD

[0001]

The present invention relates to a multilayer wiring board comprising at least two electrically connected wiring boards comprising an insulating film and wiring patterns on 10 both surfaces of the insulating film.

BACKGROUND ART

[0002]

When electronic components, for example IC chip, are 15 mounted, film carrier tapes for mounting electronic components such as TAB (tape automated bonding) tapes, CSP (chip size package) tapes, BGA (ball grid array) tapes and FPC (flexible printed circuit), laminates of these tapes, and multilayer wiring boards having rigid substrates such as glass epoxy are 20 used.

[0003]

The multilayer wiring boards are manufactured as follows. A double-sided copper clad laminate having sprocket holes is provided. Both surfaces of the laminate are coated with a

photoresist, and the photoresist layers are exposed to light and developed to form desired patterns. The copper clad laminate is then etched using the patterns as masks. Consequently, wiring patterns are formed on both surfaces of 5 the insulating substrate (film). The thus formed double-sided wiring boards are laminated through an insulating layer, and an electrical connection is established between the double-sided wiring boards. To establish electrical connections between the wiring patterns, Patent Document 1 10 (JP-A-2002-343901) discloses a process in which a bump-forming conductive material is placed in the vicinity of a substrate of a printed wiring board; the conductive material is punched, and substantially simultaneously through holes are formed in the substrate and are filled with the bump-forming conductive 15 material to form a desired number of bumps in the substrate; and a plurality of printed wiring board units are laminated via connection parts and are pressure bonded under heating to manufacture CSP.

[0004]

20 In the above process, the bump-forming conductive material and the substrate are punched out substantially at the same time, and consequently through holes are formed and are simultaneously filled with the bump-forming conductive material. The wiring patterns on both surfaces of the

insulating substrate have a very good electrical connection.

However, laminating the printed wiring board units often results in failure of reliable electrical connection between the printed wiring board units through the bump-forming

5 conductive material filled in the through holes. Namely, the bump-forming conductive material filled in the through holes is often incapable of achieving an adequate electrical connection with the surface of the wiring patterns of the mating printed wiring board units. It is therefore difficult that  
10 a laminate of such printed wiring board units achieve a stable electrical connection between the units. Providing a stable connection entails very complicated steps, and efficient production of reliable multilayer wiring boards is difficult.

[0005]

15 The laminate described above includes a plurality of the printed wiring board units with an insulating layer in between. The insulating layers used in the laminates have shown unsatisfactory properties. For example, when a high-frequency current is applied to the laminates, properties  
20 of the insulating layers are often responsible for deteriorating characteristics of the multilayer wiring boards.

[0006]

In particular, the multilayer wiring boards having

polyimide insulating substrates are often strained by the internal stress which is a result of the curing of insulating adhesives used in laminating the printed wiring board units. If the insulating adhesives have low insulating properties, 5 sufficient insulation may not be obtained when a high-frequency current is applied. As described above, the conventional processes have been incapable of ensuring an electrical connection between the printed wiring board units of the multilayer wiring board. Furthermore, concerning the 10 insulating adhesives for laminating the printed wiring board units, it must be selected in view of characteristics and use of current electronic components and must be selected such that the electrical connection between the printed wiring board units will be ensured.

15 [0007]

Patent Document 2 (JP-A-H11-163529), Patent Document 3 (JP-A-H11-163213) and Patent Document 4 (JP-A-2002-76557) disclose other types of multilayer wiring boards. However, they require very intricate production steps and are not suited 20 for the industrial mass production of stable multilayer wiring boards.

[0008]

As described above, the conventional multilayer wiring boards entail many and complicated steps for laminating a

substrate having wiring patterns thereon, and hardly achieve a stable electrical connection between the wiring boards. Manufacturing of the stable multilayer wiring boards is not necessarily easy.

5 Patent Document 1: JP-A-2002-343901

Patent Document 2: JP-A-H11-163529

Patent Document 3: JP-A-H11-163213

Patent Document 4: JP-A-2002-76557

10 **DISCLOSURE OF THE INVENTION**

**PROBLEMS TO BE SOLVED BY THE INVENTION**

[0009]

It is an object of the present invention to provide a multilayer wiring board that is easily producible by  
15 laminating wiring boards and has a reliable electrical connection between the wiring boards.

[0010]

Specifically, it is an object of the present invention to provide a multilayer wiring board having a reliable  
20 electrical connection between the wiring boards, and having a reliable bonding of the double-sided wiring boards, which maintains high characteristics even when a high frequency is applied.

**MEANS FOR SOLVING THE PROBLEMS**

[0011]

A multilayer wiring board according to the present invention comprises at least two wiring boards,

5 each of the wiring boards comprising an insulating substrate and a wiring pattern which comprises a conductive metal,

10 at least one of the at least two wiring boards having the wiring patterns on both surfaces of the insulating substrate,

at least part of the wiring patterns on the insulating substrate being connected via a conductive metal in a through hole through the insulating substrate,

15 the wiring boards being electrically connected by joining of low-melting conductive metal layers on connection terminals at the mating surfaces of the wiring boards, and the at least two wiring boards being bonded by means of a polyimide adhesive resin that is selectively applied by screen printing on the wiring boards other than on the 20 connection terminals.

[0012]

A multilayer wiring board according to the present invention comprises at least two double-sided wiring boards, each of the double-sided wiring boards comprising an

insulating substrate and wiring patterns which comprises a conductive metal on both surfaces of the insulating substrate,

the wiring patterns on the insulating substrate being connected via a conductive metal in a through hole through the 5 insulating substrate,

the double-sided wiring boards being electrically connected by joining of low-melting conductive metal layers on connection terminals at the mating surfaces of the double-sided wiring boards, and

10 the at least two double-sided wiring boards being bonded by means of a polyimide adhesive resin that is selectively applied by screen printing on the double-sided wiring boards other than on the connection terminals.

[0013]

15 In the present invention, at least two double-sided wiring boards may be laminated. The outer surface of the outermost wiring board may be free from a wiring pattern. That is, the present invention includes an embodiment in which the multilayer wiring boards have an odd number of wiring patterns, 20 for example three or five wiring patterns, across the thickness.

[0014]

In the present invention, the double-sided conductive substrate comprises the insulating film such as a polyimide

film that is sandwiched between conductive metal layers such as copper layers. Preferably, the electrical conduction between both surfaces of the double-sided conductive substrate is established by a series of steps in which a conductive metal 5 foil such as a copper foil is placed on the substrate and is punched out, and the conductive metal foil pieces punched out punch out the double-sided conductive substrate and are inserted in the double-sided conductive substrate.

Alternatively, the electrical conduction is preferably made 10 by a series of steps in which the insulating substrate or the double-sided metal clad laminate is previously provided with through holes; a conductive metal foil is placed on the substrate or laminate and is punched out; and the conductive metal pieces punched out are inserted in the through holes in 15 the insulating substrate or the double-sided metal clad laminate.

[0015]

In the multilayer wiring board of the present invention, the electrical connection between the double-sided wiring 20 boards preferably takes place at locations where the conductive metal foil pieces are inserted for electrically connecting the two surfaces of each wiring board. Low-melting conductive metal layers are formed on connection surfaces, and a specific polyimide adhesive resin is applied selectively by

screen printing. The double-sided wiring boards are pressure bonded under heating to produce a multilayer wiring board reliably.

5

**EFFECTS OF THE INVENTION**

[0016]

According to the present invention, the multilayer wiring board having high reliability can be obtained by very simple steps. That is to say, the multilayer wiring board in 10 which the wiring patterns on both surfaces of the insulating substrate are electrically connected through the conductive metal pieces inserted in the via holes is producible very easily.

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**BRIEF DESCRIPTION OF THE DRAWINGS**

[0017]

Fig. 1 is a sectional view illustrating wiring boards in steps of producing a multilayer wiring board according to the present invention;

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Fig. 2 is a sectional view in which via holes are formed in an insulating substrate and metal pieces are inserted in the via holes, and thereafter conductive metal layers are formed and patterned to form wiring patterns;

Fig. 3 is a sectional view in which via holes are formed

in an insulating substrate having conductive metal layers on both surfaces and metal pieces are inserted in the via holes to establish an electrical connection between the two surfaces of the insulating substrate;

5 Fig. 4 is a schematic sectional view of a multilayer wiring board produced in Example 2;

Fig. 5 is a schematic sectional view of a multilayer wiring board produced in Example 3;

10 Fig. 6 is a graph showing the resistance of the multilayer wiring board produced in Example 3 across its thickness;

Fig. 7 is a schematic sectional view of a multilayer wiring board produced in Example 4; and

Fig. 8 is a graph showing the resistance of the multilayer wiring board produced in Example 4 across its thickness.

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#### DESCRIPTION OF CODES

[0018]

10 ... Insulating substrate

12a, 12b ... Conductive metal layer

20 13 ... Double-sided metal clad laminate

14a, 14b ... Pattern

15a, 15b ... Wiring pattern

20 ... Double-sided wiring board

20-1, 20-2 ... Double-sided wiring board

21 ... Through hole  
22 ... Conductive metal piece  
25 ... Conductive metal foil  
30 ... Punch  
5 30a, 30b, 30c, 30d ... Connection terminal (wiring pattern)  
33 ... Low-melting conductive metal layer  
34 ... Connection metal layer  
35-1, 35-2 ... Adhesive layer  
35 ... Adhesive layer  
10 42a, 42b ... Conductive metal layer  
43 ... Double-sided metal clad laminate  
50 ... Multilayer wiring board

**BEST MODE FOR CARRYING OUT THE INVENTION**

15 [0019]

The multilayer wiring boards according to the present invention will be described with reference to the figures.

[0020]

Fig. 1 is a sectional view illustrating wiring boards  
20 in steps of producing a multilayer wiring board according to the present invention. Figs. 2 and 3 are sectional views illustrating composite substrates used for the manufacturing of the multilayer wiring board according to the present invention.

[0021]

As shown in Figs. 1 and 2, a double-sided metal clad laminate 13 comprises an insulating substrate 10 and conductive metal layers 12a and 12b on both surfaces of the substrate. The conductive metal layers 12a and 12b on the insulating substrate 10 are selectively etched, and consequently wiring patterns 15a and 15b are formed on both surfaces of the insulating substrate 10. At least two such double-sided wiring boards 20 are laminated.

10 [0022]

The double-sided wiring board 20 of the present invention has through holes 21 that establish electrical conduction between the two surfaces of the insulating substrate 10. Conductive metal pieces 22 are inserted in the through holes 21. Consequently, the wiring patterns 15a and 15b on the front and back surfaces of the insulating substrate 10 are electrically connected at locations required.

[0023]

The conductive metal pieces 22 may be inserted in the through holes 21 in the insulating substrate 10 as illustrated in Fig. 2. A conductive metal foil 25 is placed on the surface of the insulating substrate 10. The conductive metal foil 25 and the insulating substrate 10 are punched with punches 30 simultaneously such that the conductive metal pieces 22 to be

inserted in the insulating substrate 10 will be punched out and will function as tips of the punches to punch out the insulating substrate 10 and to form the through holes 21 in the insulating substrate 10, and the pieces 22 will remain in 5 the through holes 21 in the insulating substrate 10. The conductive metal pieces 22 remaining in the through holes 21 work as means for electrically connecting wiring patterns 15a and 15b that will be formed on both surfaces of the insulating substrate 10. The punches for forming the through holes 21 10 are approximately from 1 to 1000  $\mu\text{m}$ , preferably from 10 to 500  $\mu\text{m}$  in diameter, whereby very fine through holes are formed. The conductive metal foil 25 has a thickness equal to or slightly greater than that of the insulating substrate 10. The electrical conduction across the thickness of the insulating 15 substrate may be alternatively established as follows. The insulating substrate 10 is perforated with punches or the like to form through holes. The conductive metal foil 25 is placed on the perforated insulating substrate 10 and is punched with the punches 30 such that the conductive metal pieces 22 to be 20 inserted in the insulating substrate 10 will be punched out and will remain in the through holes in the insulating substrate 10. The conductive metal pieces work as means for electrically connecting wiring patterns that will be provided on both surfaces of the insulating substrate 10.

[0024]

The insulating substrates 10 used in the present invention may be synthetic resin films having excellent heat resistance, chemical resistance, and humidity and heat 5 stability. Examples of the synthetic resin films include polyimide films, polyamideimide films, heat-resistant polyester films, BT resin films, phenolic resin films and liquid crystal polymer films. Of these, in the present invention polyimide films are preferable because of their 10 prominent heat resistance, chemical resistance, and humidity and heat stability. The insulating substrate 10 generally has a thickness of 5 to 150  $\mu\text{m}$ , preferably 5 to 125  $\mu\text{m}$ . The conductive metal foil 25 placed on the insulating substrate 10 has a thickness equal to or slightly greater than that of 15 the insulating substrate 10. Specifically, the conductive metal foil 25 generally has a thickness of 50 to 200  $\mu\text{m}$ , preferably 80 to 120  $\mu\text{m}$ . That is, the conductive metal foil 25 is generally 100 to 300% thicker, preferably 200 to 240% thicker than the insulating substrate 10. When the slightly 20 thicker conductive metal foil 25 is used, both ends of the conductive metal pieces 22 slightly protrude from the surfaces of the insulating substrate 10. The exposed protrusions can be caulked to prevent detachment of the conductive metal pieces 22 from the through holes 21.

[0025]

After the conductive metal pieces 22 are inserted in the through holes 21 formed in the insulating substrate 10, the conductive metal layers 12a and 12b are formed over the surface 5 of the insulating substrate 10 to cover the conductive metal pieces 22. The conductive metal layers 12a and 12b may be formed by laminating conductive metal foils on the insulating substrate 10. Alternatively, the surfaces of the insulating substrate 10 may be plated with a conductive metal such as 10 copper or aluminum by using plating technique. Moreover, the conductive metal layers 12a and 12b may be formed by depositing a conductive metal on the surfaces of the insulating substrate 10 by using deposition technique. The conductive metal layers 12a and 12b may be single layers of a conductive metal or 15 laminates of a plurality of conductive metal layers.

[0026]

Fig. 3 shows another embodiment of the present invention. A double-sided metal clad laminate 43 is provided which comprises an insulating substrate 10 and conductive metal 20 layers 42a and 42b on the surface of the insulating substrate. A conductive metal foil 25 is placed on the surface of the double-sided metal clad laminate 43. The conductive metal foil 25 and the double-sided metal clad laminate 43 are punched with punches 30 simultaneously such that conductive metal

pieces 22 to be inserted in the double-sided metal clad laminate 43 will be punched out and will function as tips of the punches 30 to punch out the double-sided metal clad laminate 43 and to form through holes 21 in the double-sided metal clad laminate 5 43, and the pieces 22 will remain in the through holes 21 in the double-sided metal clad laminate 43. The conductive metal pieces 22 remaining in the through holes 21 electrically connect the conductive metal layers 42a and 42b on both surfaces of the insulating substrate 10. Subsequently, the board is 10 plated with copper or the like in a thickness of 3 to 6  $\mu\text{m}$  to enhance connection reliability between the conductive metal layers and the conductive metal pieces 22. The plating metals include nickel, solder, lead-free solder and tin.

[0027]

15 The double-sided metal clad laminate 43 may be manufactured by laminating conductive metal foils on both surfaces of the insulating substrate, or by depositing conductive metals on both surfaces of the insulating substrate by using plating or deposition. The conductive metal layers 20 may be single layers of a conductive metal such as copper, copper alloy or aluminum, or may be laminates of a plurality of different conductive metal layers. The electrical conduction across the thickness of the insulating substrate of the present invention may be alternatively established as

follows. The double-sided metal clad laminate 43 is perforated with punches or the like to form through holes. The conductive metal foil 25 is placed on the perforated laminate and is punched with the punches 30 such that the conductive 5 metal pieces 22 are punched out and are inserted in the through holes 21 in the double-sided metal clad laminate 43. The conductive metal pieces 22 remaining in the through holes 21 work as means for electrically connecting the conductive metal layers 42a and 42b on both surfaces of the insulating substrate 10 10.

[0028]

The conductive metal layers 12a, 12b, 42a and 42b thus formed are generally from 4 to 35  $\mu\text{m}$ , preferably from 6 to 15  $\mu\text{m}$  in thickness.

15 [0029]

The double-sided wiring boards 20 for manufacturing a multilayer wiring board 50 of the present invention are produced as follows. Using the double-sided metal clad laminates 13 having the conductive metal layers 12a and 12b 20 on both surfaces, or the double-sided metal clad laminates 43 having the conductive metal layers 42a and 42b on both surfaces, for example, photoresist layers are formed on the conductive metal layers 12a and 12b as shown in Fig. 2, and are exposed to light and developed to form photoresist patterns 14a and

14b on the conductive metal layers 12a and 12b. The conductive metal layers 12a and 12b are selectively etched using the patterns 14a and 14b as masks. Referring to Fig. 2, the wiring patterns 12a and 12b on the front and back surfaces of the 5 insulating substrate 10 are electrically connected through the conductive metal pieces 22 filled in the insulating substrate 10.

[0030]

The multilayer wiring board 50 according to the present 10 invention comprises at least two double-sided wiring boards 20. Fig. 1 illustrates lamination of two double-sided wiring boards 20-1 and 20-2.

[0031]

The double-sided wiring board 20-1 on the right side in 15 Fig. 1 has the wiring pattern 15b on the back surface, to which the double-sided wiring board 20-2 on the left side is laminated. Specifically, a wiring (connection terminal) 30d and a wiring (connection terminal) 30e are to be connection terminals. The double-sided wiring board 20-2 has the wiring pattern 15a on 20 the front surface, to which the mating wiring board is laminated. Specifically, a wiring (connection terminal) 31d and a wiring (connection terminal) 31c are to be connection terminals.

[0032]

To establish an electrical connection between the

double-sided wiring boards 20-1 and 20-2 that are laminated, low-melting conductive metal layers 33 are formed on the surface of the connection terminals 30d and 30e on the back surface of the double-sided wiring board 20-1, and the surface 5 of the connection terminals 31a and 31b on the front surface of the double-sided wiring board 20-2. The low-melting conductive metal layers 33 are generally composed of a metal or alloy having a melting point of not more than 300°C, preferably from 180 to 240°C. Examples of the low-melting 10 metals and alloys include solder, lead-free solder, tin, gold and nickel-gold. The low-melting conductive metal layers 33 may include one or more metals and alloys in combination. That is, the low-melting conductive metal layers 33 may be single layers of these metals or alloys, or laminates of a plurality 15 of such layers.

[0033]

The low-melting conductive metal layers 33 of the above metals or alloys may be formed on the connection terminals 30d, 30e, 31a and 31b by various methods. In the present invention, 20 plating is advantageous for forming the low-melting conductive metal layers 33. When forming the low-melting conductive metal layers 33 by plating, the surface of the wiring patterns 15a and 15b that are on the double-sided wiring boards 20-1 and 20-2 and do not participate in the electrical connection

between the double-sided wiring boards 20-1 and 20-2 is preferably protected by resin films or the like. That is to say, the connection terminals 30d and 30e, and the connection terminals 31a and 31b are selectively exposed from the surface 5 of the double-sided wiring boards 20-1 and 20-2, and the other area is coated with the resin, followed by plating. The selective application of the protective resin may be performed using screen masks masking the connection terminals 30d and 30e, and the connection terminals 31a and 31b. According the 10 present invention, the protective resin may be a polyimide adhesive resin, which is used for forming adhesive layers as will be described later. It is preferable that the polyimide adhesive resin is applied through screen masks as described, and is cured temporarily by heating.

15 [0034]

The connection terminals 30d and 30e, and the connection terminals 31a and 31b are selectively exposed from the surface of the double-sided wiring boards 20-1 and 20-2 as described above. The double-sided wiring boards 20-1 and 20-2 are 20 immersed in a plating solution containing a desired metal, and the connection terminals 30d and 30e, and the connection terminals 31a and 31b are plated, resulting to form the low-melting conductive metal layers 33. Particularly preferably, in the present invention the low-melting

conductive metal layer 33 is at least one plated metal layer selected from the group consisting of plated solder layer, plated lead-free solder layer, plated tin layer, plated gold layer and plated nickel-gold layer. Particularly, in the 5 present invention the low-melting conductive metal layer 33 is preferably a plated solder layer or a plated lead-free solder layer. The low-melting conductive metal layers 33 may be formed by electroplating or electroless plating.

[0035]

10 The thickness of the low-melting conductive metal layers 33 thus formed may be determined appropriately depending on the metal or alloy used. Generally, the thickness is in the range of 0.5 to 10  $\mu\text{m}$ , preferably 3 to 6  $\mu\text{m}$ . This thickness permits the low-melting conductive metal layers 33 to ensure 15 good electrical connection between the double-sided wiring boards 20-1 and 20-2, and prevents short-circuits by excess low-melting conductive metal in establishing the electrical connection.

[0036]

20 The first conductive metal layers are formed on the electrical connection surface of the double-sided wiring board 1. The second conductive metal layers are formed on the electrical connection surface of the mating double-sided wiring board that is to be electrically connected with the

double-sided wiring board 1. Preferably, the first and the second conductive metal layers have at least one combination selected from the group consisting of plated solder layers/plated nickel-gold layers, plated tin layers/plated 5 nickel-gold layers, plated solder layers/plated solder layers, plated tin layers/plated nickel-gold layers, plated lead-free solder layers/plated lead-free solder layers, plated lead-free solder layers/gold paste layers, and plated gold layers/plated gold layers. Particularly, the combinations of 10 plated solder layers/plated solder layers, plated solder layers/plated nickel-gold layers, and plated tin layers/plated nickel-gold layers are preferred.

[0037]

When the resin films have been provided for the purpose 15 of protection, they are peeled after the low-melting conductive metal layers 33 are formed as described above.

[0038]

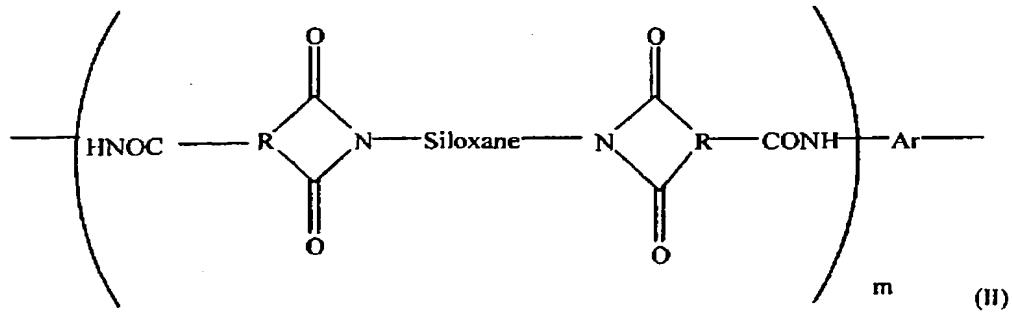
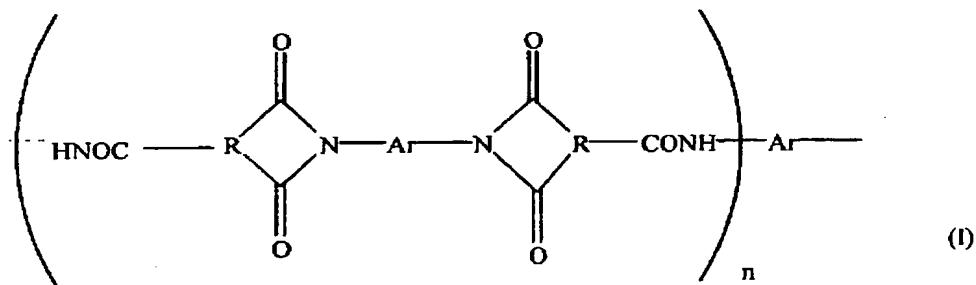
The low-melting conductive metal layers 33 are formed on the connection terminals 30d and 30e, and the connection 20 terminals 31a and 31b as described above. Subsequently, adhesive layers 35-1 and 35-2 are formed on mating surfaces at which the double-sided wiring boards 20-1 and 20-2 are bonded. Namely, the adhesive layers 35-1 and 35-2 are formed such that the connection terminals 30d and 30e will be exposed on the

back surface of the double-sided wiring board 20-1 and the connection terminals 31a and 31b will be exposed on the front surface of the double-sided wiring board 20-2. The adhesive used in the present invention is a polyimide adhesive resin.

5 The polyimide adhesive resin of the present invention contains hard segments having a polyimide group, and soft segments which bind the hard segments. The hard segment is a typical aromatic polyimide skeleton represented by Formula (I) below. The soft segment is a siloxane polyimide skeleton represented by

10 Formula (II) below.

[0039]



[0040]

In Formulae (I) and (II), R is a hydrocarbon group, Ar is an aromatic group, Siloxane is a siloxane-derived group, and m and n are each an arbitrary integer.

[0041]

5 The polyimide adhesive resins generally have a weight-average molecular weight of about 300,000 to 150,000.

[0042]

The polyimide adhesive resin of the present invention contains a polyimide precursor and is a thermosetting resin.

10 The polyimide adhesive resin preferably has a solubility parameter in the range of 17.5 to 22.5  $(\text{MJ}/\text{m}^3)^{1/2}$ , in which the polyamide adhesive resin shows very high affinity for polyimides that are possible materials of the double-sided wiring boards. The polyimide adhesive resin (cured)

15 preferably has a tensile modulus in the range of 125 to 175 MPa, which reduces the possibility of deformed multilayer wiring board by internal stress resulting from the bonding.

The solubility parameter and tensile modulus of the polyimide adhesive resin may be controlled by the structure of the soft segments of the polyimide adhesive resin, and the number of elements constituting the main chain of the resin. Examples of the polyimide adhesive resins include SN-9000 manufactured by Hitachi Chemical Co., Ltd., and UPICOAT FS-100L and UPICOAT FS-510 manufactured by UBE INDUSTRIES, LTD. The viscosity of

the polyimide adhesive resins is preferably adjusted with methylpyrrolidone,  $\gamma$ -butyrolactone, epoxy resins and the like.

[0043]

The polyimide adhesive resin is applied to the back 5 surface of the double-sided wiring board 20-1 such that the connection terminals 30d and 30e will be exposed. The polyimide adhesive resin is applied to the front surface of the double-sided wiring board 20-2 such that the connection terminals 31a and 31b will be exposed. In the present 10 invention, it is necessary that the polyimide adhesive resin be applied such that the connection terminals will be exposed on the bonding surfaces of the double-sided wiring boards. The selective application of the polyimide adhesive resin can be performed using screen masks. Specifically, the screen masks 15 cover the areas including the connection terminals that should avoid the application of the polyimide adhesive resin, and the polyimide adhesive resin is selectively applied to desired areas. In the event that the masks used in the plating of the low-melting conductive metal layers 33 are a temporarily cured 20 polyimide adhesive resin, the temporarily cured polyimide adhesive resin layers may be used as adhesive layers.

[0044]

The polyimide adhesive resin is desirably applied in a thickness that is substantially the same level as the surface

of the connection terminals 30d and 30e, and the surface of the connection terminals 31a and 31b. The thickness (as measured after the solvent is removed) is generally from 5 to 20  $\mu\text{m}$ , preferably from 10 to 15  $\mu\text{m}$ .

5 [0045]

The adhesive layers 35-1 and 35-2 are formed on the double-sided wiring boards 20-1 and 20-2, respectively, as described above. The double-sided wiring boards are arranged such that the adhesive layers 35-1 and 35-2 are opposed and 10 further such that the connection terminals 30d and 30e on the double-sided wiring board 20-1 are faced to the connection terminals 31b and 31a on the double-sided wiring board 20-2 each other. Subsequently, the double-sided wiring board 20-1 and the double-sided wiring board 20-2 are pressed against one 15 another with heating. The heating temperature is at least the curing temperature of the polyimide adhesive resin in order that the double-sided wiring boards are bonded, and is generally in the range of 150 to 300°C, preferably 190 to 250°C. The wiring boards are pressed against one another at a pressure 20 of about 1 to 4  $\text{kg}/\text{cm}^2$  at the above temperature for 1 to 20 seconds, preferably 5 to 10 seconds. Consequently, the polyimide adhesive resin develops adhesion between the double-sided wiring boards 20-1 and 20-2 and forms an adhesive layer 35 which bonds and integrates the double-sided wiring

boards 20-1 and 20-2. The laminate in which the double-sided wiring boards 20-1 and 20-2 are bonded and integrated with the polyimide adhesive resin may be subjected to additional heating and pressing as required, whereby the bond strength 5 of the laminate may be improved.

[0046]

The heating under pressure, optionally accompanied by application of ultrasonic waves, melts the metals or alloys of the low-melting conductive metal layers 33 on the mating 10 connection terminals 30d and 31b, and the mating connection terminals 30e and 31a. Consequently, the conductive metal layers in contact with each other are unified to form connection metal layers 34. The connection metal layers 34 electrically connect the double-sided wiring boards 20-1 and 20-2.

15 [0047]

Although the above multilayer wiring board comprises two double-sided wiring boards, more wiring boards may be added by laminating double-sided wiring boards or one-sided wiring boards in a similar manner.

20 [0048]

Alternatively, wiring boards may be increased by laminating the multilayer wiring boards thus manufactured through an insulating layer. Still alternatively, a combination of the provision of an insulating resin layer,

masking and selective plating on the surface of the thus manufactured multilayer wiring board increases the number of wiring boards. Wiring boards may be added to the multilayer wiring board on which electronic components are mounted.

5 [0049]

To ensure conduction through the thickness of the multilayer wiring board, additional electrical connection means may be provided through the thickness of the multilayer wiring board. As an example, via holes may be made by punching 10 or laser beam application followed by desmearing as required, and the inner walls of the formed via holes may be plated with a conductive metal. Instead of the plating, the via holes may be filled with a conductive metal, or a conductive metal may be inserted in the via holes.

15 [0050]

Although the above embodiments are focused on the double-sided wiring boards in which the wiring patterns are formed on both surfaces of the insulating substrate, the multilayer wiring board of the present invention may have, for 20 example, two double-sided wiring boards one or both of which are free of a wiring pattern on the outermost surface of the insulating substrate.

[0051]

Various modifications to the multilayer wiring boards

of the present invention are possible.

[0052]

For example, in the above description, the electrical connection between the front and back surfaces of the 5 double-sided wiring board is established by punching the conductive metal foil and the substrate simultaneously, whereby the conductive metal pieces are punched out and are inserted in the through holes in the substrate to electrically connect the front and back surfaces of the substrate. 10 Alternatively, through holes may be made in the substrate by punching or laser beam application, and a conductive metal may be selectively deposited on the inner walls of the through holes to establish an electrical connection between the front and back surfaces of the substrate. Instead of the deposition, 15 the through holes may be filled with a conductive paste containing a large amount of a conductive metal to establish an electrical connection between the front and back surfaces of the substrate.

[0053]

20 One or more electronic components may be mounted on the double-sided wiring boards in which the wiring patterns are formed on both surfaces of the insulating substrate.

[0054]

When the double-sided wiring boards of the present

invention are flexible tapes, the tapes may be provided with sprocket holes along the edges on both sides so that the tapes can be transferred. Positioning holes may be provided for alignment.

5 [0055]

The wiring patterns on the surface of the multilayer wiring boards of the present invention may be surface treated as required, for example by plating. The wiring patterns may be protected with a solder resist layer while exposing the 10 terminals. The multilayer wiring boards may be provided with outer terminals such as outer leads and outer pads.

[0056]

The multilayer wiring boards can be used for the mounting of electronic components.

15 [0057]

According to the present invention, a plurality of double-sided wiring boards may be easily laminated while establishing highly reliable electrical connection between the wiring boards. The multilayer wiring boards of the present 20 invention have high reliability.

#### INDUSTRIAL APPLICABILITY

[0058]

According to the present invention, the multilayer

wiring board having high reliability may be obtained through very simple steps. That is to say, the wiring patterns on both surfaces of the insulating substrate are electrically connected through the conductive metal pieces inserted in the 5 via holes. The multilayer wiring board is producible very easily. Specifically, the electrical connection between the double-sided wiring boards is established through the plated layers made of specific low-melting conductive metals. The plated layers of low-melting conductive metals ensure 10 electrical connection through the thickness of the multilayer wiring board. The double-sided wiring boards are laminated by means of a specific polyimide adhesive resin, and consequently the multilayer wiring board is not deformed and achieves high reliability.

15

#### EXAMPLES

[0059]

The multilayer wiring boards according to the present invention will be described in more detail by Examples without 20 limiting the scope of the present invention.

Example 1

[0060]

An insulating substrate was a polyimide film 50  $\mu\text{m}$  in thickness. The polyimide film had copper layers 12  $\mu\text{m}$  in

thickness on both surfaces. This double-sided copper clad laminate (35 mm wide) was provided with sprocket holes along the edges on both sides in the width direction.

[0061]

5        The double-sided copper clad laminate (total thickness: 74  $\mu\text{m}$ ) was perforated to produce punching holes 100  $\mu\text{m}$  in diameter. A rolled copper foil having an average thickness of 100  $\mu\text{m}$  was overlaid on the surface of the laminate, and the rolled copper foil was punched with punches 100  $\mu\text{m}$  in diameter.

10      The pieces of the rolled copper foil punched out were inserted to remain in the punching holes. Consequently, the front and back surfaces of the double-sided copper clad laminate were electrically connected.

[0062]

15      After the pieces punched out were inserted in the punching holes, the copper layers of the double-sided copper clad laminate were plated with copper in a thickness of 3  $\mu\text{m}$ . Then, a photoresist was applied to the plated copper layers and exposed to light and developed to form desired patterns.

20      [0063]

      The plated copper layers were selectively etched using the patterns as masks, and wiring patterns were formed on both surfaces of the double-sided copper clad laminate. The wiring patterns included the punching holes in which the pieces

punched out were inserted. Consequently, the wiring patterns were electrically connected through the pieces.

[0064]

A polyimide adhesive resin (SN-9000 manufactured by 5 Hitachi Chemical Co., Ltd.) was applied through screen masks such that parts of the wiring patterns would be exposed. The exposed parts of the wiring patterns included the punching holes on the connection surfaces of the double-sided wiring board and were capable of electrical connection when boards 10 are laminated. The polyimide adhesive resin was applied such that the dry thickness would be 15  $\mu\text{m}$ . The polyimide adhesive resin was heated at 120°C for 5 minutes, and was temporarily cured. The double-sided wiring board masked with the temporarily cured polyimide adhesive resin was immersed in a 15 solder plating bath. Consequently, the parts of the wiring patterns for electrical connection were plated with a low-melting conductive metal, namely solder, in a thickness of 3  $\mu\text{m}$ .

[0065]

20 Two double-sided wiring boards were arranged such that the temporarily cured polyimide adhesive resin layers would be faced to each other. The polyimide adhesive resin was cured by heating at 250°C for 10 seconds. Consequently, the wiring boards were bonded together and the plated solder layers that

were connection terminals were molten to establish an electrical connection between the wiring boards.

[0066]

5       The polyimide adhesive resin contained hard segments forming polyimide bonds, and soft segments with siloxane bonds represented by Formula (II) above that bound the polyimide bonds. The polyimide adhesive resin was separately measured for a dielectric constant of cured product, resulting in  $1 \text{ MHz} : \epsilon = 3.38$  and  $\text{Tan}\delta = 0.019$ . The polyimide adhesive resin had a  
10      solubility parameter of  $19 \text{ (MJ/m}^3\text{)}^{1/2}$  and a tensile modulus of 140 MPa. The polyimide adhesive resin was separately measured for a bonding strength with respect to a polyimide film, resulting in 450 g/25 mm.

[0067]

15       The multilayer wiring board produced as above had little resistance variation between the front and back surfaces, and proved very high reliability.

Example 2

[0068]

20       A multilayer wiring board as shown in Fig. 4 was manufactured in the same manner as in Example 1. The multilayer wiring board was subjected to a corrosion resistance test (PCT test: 2.5 atm, 127°C, 100% RH, 120 hr), a temperature characteristic test 1 (hot oil test: 10 cycles

of 260°C (5 sec) and 23°C (15 sec)), and a temperature characteristic test 2 (reflow test: 3 cycles of 260°C (10 sec)). Changes of resistance across the thickness of the multilayer wiring board were measured.

5 [0069]

100 samples were measured for resistance before and after the tests. An objective change of resistance was not more than 10 mΩ/via hole. All the samples showed resistance changes within the range of ±10%. The results of the PCT test, hot 10 oil test and reflow test of the 100 samples are given in Table 1.

[0070]

[Table 1]

Test Item	Resistance change after test
PCT test	10%
Hot oil test	5%
Reflow test	6%

15 Example 3

[0071]

A double-sided wiring board with a plated nickel-gold layer, and a double-sided wiring board with a plated solder layer were laminated together, and electrical connection was

established in the same manner as in Example 1. Resultant multilayer wiring board is shown in Fig. 5.

[0072]

The multilayer wiring board was measured for resistance 5 across thickness. An objective resistance variation was not more than  $10 \text{ m}\Omega$ . The results are shown in Fig. 6.

[0073]

As shown in Fig. 6, the average electrical resistance was  $2.25 \text{ m}\Omega$ , with  $3.66 \text{ m}\Omega$  maximum and  $1.92 \text{ m}\Omega$  minimum. The 10 double-sided wiring boards had little resistance variation and proved excellent electrical properties.

Example 4

[0074]

A double-sided wiring board with a plated tin layer, and 15 a double-sided wiring board with a plated nickel-gold layer were laminated together, and electrical connection was established in the same manner as in Example 1. Resultant multilayer wiring board is shown in Fig. 7.

[0075]

20 The multilayer wiring board was measured for resistance across thickness. An objective resistance variation was not more than  $10 \text{ m}\Omega$ . The results are shown in Fig. 8.

[0076]

As shown in Fig. 8, the average electrical resistance was  $3.75 \text{ m}\Omega$ , with  $5.96 \text{ m}\Omega$  maximum and  $1.19 \text{ m}\Omega$  minimum. The double-sided wiring boards had little resistance variation and proved excellent electrical properties.